

# Redesign of Cartesian Diver for Underwater Expression Combining Dynamic Fabrication with Non-Contact Manipulation

Amy Koike, Kazuki Takazawa, Satoshi Hashizume,  
Mose Sakashita, Daitetsu Sato, and Yoichi Ochiai

University of Tsukuba  
amy23kik@gmail.com

**Abstract.** In this study, we aim to combine dynamic fabrication with non-contact manipulation system applying the mechanism of Cartesian Diver. To achieve this, we propose the design method for underwater objects and non-contact manipulation technique using water pressure with PID control. We successfully designed and manipulate the object by our method. We discussed the principles and methods to create a digitally designed and fabricated the diver and to stabilize it in the middle of water.

**Keywords:** Dynamic Fabrication; PIDcontrol; Cartesian Diver; Underwater

## 1 Introduction

Cartesian Diver is known as a toy which swims up and down underwater. The diver is often used as demonstration of Pascal's law and Archimedes's principle. It uses the change of water pressure and specific structure to swim objects underwater situation. In this paper, we computationally design the diver in the context of dynamic fabrication and non-contact manipulation. Thus, this work expands the expressions of underwater entertainment situation such as aquarium or theme park.

Dynamic fabrication is one of the widely spreading research topic in Human Computer Interaction (HCI) communities. Some dynamic fabrication studies, for example, balanced models [8], spinnable objects [1] and floating objects [13], are proposed. More recently, Prévost et al. presented a bistable balanced object using movable embedded masses [7]. This study is one of example which enhance the degree of freedom in dynamic fabrication. Moreover, there are some methods adding controllability to fabricated objects using non-contact manipulation systems; controlling magnetic field [5], acoustic field [6] or air jets [4].

In this work, we aim to combine dynamic fabrication with non-contact manipulation system applying the mechanism of the diver. Our contributions are

- to propose the design method for underwater objects,
- to propose the non-contact underwater object manipulation method and implementation and
- to conduct quantitative evaluation about relationship between parameter of fabrication and stability of manipulation.

## 2 Related Work

### 2.1 Fabrication

In HCI communities, optimization algorithms and digital fabrication techniques are frequently used for adding controllable physical properties to the real-world objects. These methods are applied to various targets, such as musical instruments [12][11], mechanical toys [2][14][15], and toys-redesigning [9][10].

Prévost et al., Bächer et al., and Wang et al. applied voxel carving for controlling the center of mass to balancing objects [8], spinnable objects [1] and floating objects [13]. Moreover, Prévost et al. presents a bistable balanced objects using embedded movable masses [7]. In this study, we combined underwater non-contact manipulation system with dynamic fabrication for adding spatial controllability to underwater objects.

### 2.2 Manipulation

The methods to control the real-world objects are categorized into two types. Putting actuators inside the objects or actuating their surroundings such as air or water. The latter method is also divided to two ways; contact or non-contact.

Follmer et al. proposed contact manipulation system using shape-changing display [3]. Examples of non-contact manipulation include magnetic field [5], acoustic field [6], and air jets [4].

In this study, we introduce underwater non-contact manipulation technique using water pressure with PID control.

## 3 Design Method

To design a 3D model to function as the diver, we define four fundamental requirements. To swim up and down underwater situation, the diver

1. has to float when you put it into a water tank and
2. is necessary to have a hole which water enters into it when water pressure is applied to the water tank.

To make the diver swim with the correct orientation which defined by the designer,

3. the hole is located on the same vertical line with center of gravity and
4. rotation moments should not be occurred.

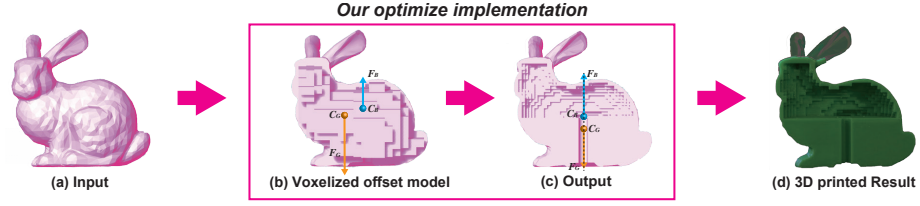
We formulated these requirements for applying them to digital fabrication system. Requirements 1. and 2. are formulated as:

$$\mathbf{F}_G + \rho_w V_{max} \mathbf{g} > \mathbf{F}_B > \mathbf{F}_G \quad (1)$$

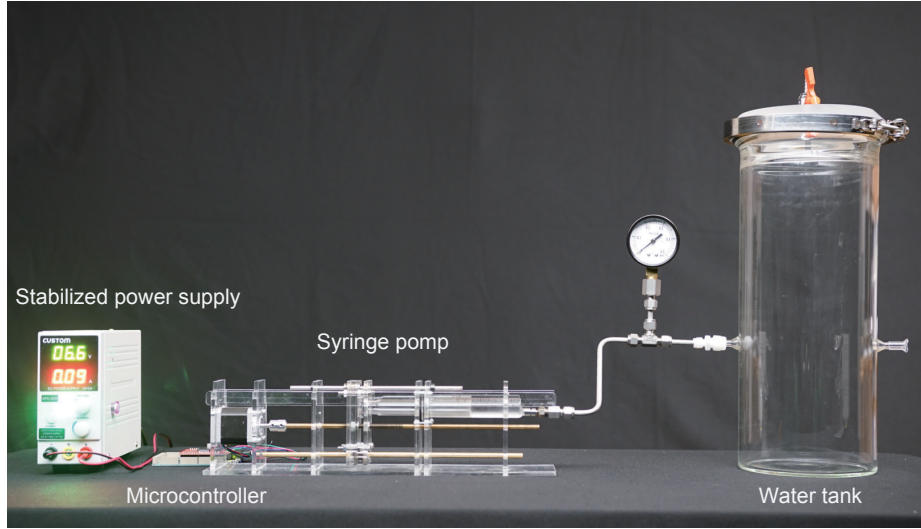
where  $\mathbf{F}_G$  is the gravitational force on the object and  $\mathbf{F}_B$  is the upward buoyancy force.  $V_{max}$  is maximum volume of water that our setup can apply to the diver,  $\rho_w$  is water density and  $g$  is gravitational acceleration. Also, requirements 3. and 4. are formulated as:

$$\mathbf{C}_B \times \mathbf{F}_B = \mathbf{C}_G \times \mathbf{F}_G \quad (2)$$

where  $\mathbf{C}_G$  is the center of gravity and  $\mathbf{C}_B$  is the center of buoyancy. Figure 1 shows our design method overview.



**Fig. 1.** Overview of our design method to create the Cartesian Diver. (a) First, we prepare a solid model as input. (b) Second, offset the model and voxelize it. (c) Then, apply voxel carving algorithm and (d) the model is 3D printed as the diver.



**Fig. 2.** System setup.

## 4 Manipulation method and system setup

To manipulate the position of the diver, we adopt PID control and implement the system setup (Figure 2).

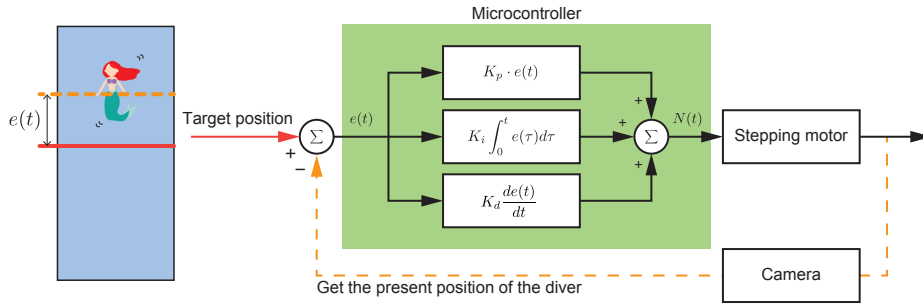
Our system consists of a water tank which is connected to a syringe pump by a tube. The syringe pump moves forward or backward by a stepping motor. The motor is controlled by a microcontroller. When it works, water pressure inside the tank is changed and it comes to decrease or increase the buoyant force applied to the diver. We installed a camera to track the position of the diver and send the value to the microcontroller.

Besides changing the water pressure, there are several ways to manipulate the diver; changing the temperature of the liquid or using two kinds of liquid each density is different. However, these methods have disadvantages of responsiveness and interactivity.

In this study, therefore, we adopt PID control to manipulate the diver. PID control can be expressed mathematically as:

$$N(t) = K_p e(t) + K_i \int_0^t e(\tau) d\tau + K_d \frac{de(t)}{dt} \quad (3)$$

where  $N(t)$  is rotational speed of the stepping motor,  $K_p$  is a factor of proportionality,  $K_i$  is integration constant and  $K_d$  is differential constant. Also,  $e(t)$  indicates difference between a target position and the present position of the diver. Figure 3 shows pipeline of PID control.



**Fig. 3.** Block diagram of PID control.

## 5 Result

### 5.1 Fabrication

We fabricated a variety of the divers and attained a result that they swim up and down in the correct orientation. However, it has limitation about material properties; water solubility and density.

Due to manipulate the diver underwater, we cannot use water soluble materials as 3D printing material. In this study, we do not consider a material which density lighter than water because it is rarely used in 3D printing.

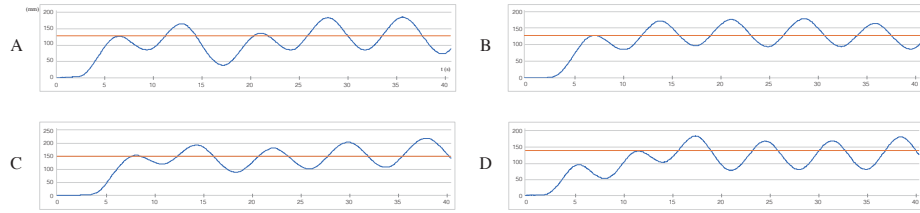
### 5.2 Manipulation

We observed the position deviation of the diver under applying PID control. Gravity, buoyancy, and fluid resistance are applied to the diver while the diver is moving. Fluid resistance  $F_D$  is defined by the properties of the fluid, the shape, and the speed of the object:

$$F_D = \frac{1}{2} \rho v^2 C_D S \quad (4)$$

where  $\rho$  is the density of the fluid,  $v$  is the speed of the object relative to the fluid,  $C_D$  is the drag coefficient and  $S$  is the cross sectional area. The cross sectional area is defined as orthographic projection toward direction of movement of the object. Therefore we examined effectiveness of the cross sectional area of the diver to stability under the control (Figure 4).

Under the control, the object oscillate near the target position. It is caused by two system setup factors; frictional force applied to the syringe pump and image processing delay. We need to improve the system setup to decrease these factors in the future work.



**Fig. 4.** These graphs show behavior of four Cartesian Divers under PID control. Those cross sectional area are different; A is  $425\pi$ , B is  $400\pi$ , C is  $350\pi$  and D is  $300\pi$ . Those volume ( $62800\text{mm}^3$ ) and the material (3D printed PLA) are same. Red line is the target position.

## 6 Conclusion

In this study, we aim to combine dynamic fabrication with non-contact manipulation system. To achieve this, we proposed the design methods applying the mechanism of Cartesian Diver.

We successfully design and manipulate the diver and discussed limitations. We observed the motion of the diver under applying PID control. Then we discussed about limitation about material properties and system setup. We believe this study extends the possibilities of new underwater expressions.

## References

1. Moritz Bächer, Emily Whiting, Bernd Bickel, and Olga Sorkine-Hornung. 2014. Spin-it: Optimizing Moment of Inertia for Spinnable Objects. *ACM Trans. Graph.* 33, 4, Article 96 (July 2014), 10 pages. DOI:<http://dx.doi.org/10.1145/2601097.2601157>
2. Stelian Coros, Bernhard Thomaszewski, Gioacchino Noris, Shinjiro Sueda, Moira Forberg, Robert W. Sumner, Wojciech Matusik, and Bernd Bickel. 2013. Computational Design of Mechanical Characters. *ACM Trans. Graph.* 32, 4, Article 83 (July 2013), 12 pages. DOI: <http://dx.doi.org/10.1145/2461912.2461953>
3. Sean Follmer, Daniel Leithinger, Alex Olwal, Akimitsu Hogge, and Hiroshi Ishii. 2013. in-FORM: Dynamic Physical Affordances and Constraints Through Shape and Object Actuation. In *Proceedings of the 26th Annual ACM Symposium on User Interface Software and*

- Technology (UIST '13)*. ACM, New York, NY, USA, 417–426. DOI:<http://dx.doi.org/10.1145/2501988.2502032>
4. M. Hiroshi, Y. Yoshihiro, I. Satoshi, S. Motoki, N. Toshiro, S. Yuriko, K. Minoru, and Y. Masanori. 2010. Contactless active force closure manipulation using multiple air jets. In *2010 IEEE International Conference on Systems, Man and Cybernetics*. 4154–4160. DOI:<http://dx.doi.org/10.1109/ICSMC.2010.5642402>
  5. Jinha Lee, Rehmi Post, and Hiroshi Ishii. 2011. ZeroN: Mid-air Tangible Interaction Enabled by Computer Controlled Magnetic Levitation. In *Proceedings of the 24th Annual ACM Symposium on User Interface Software and Technology (UIST '11)*. ACM, New York, NY, USA, 327–336. DOI:<http://dx.doi.org/10.1145/2047196.2047239>
  6. Yoichi Ochiai, Takayuki Hoshi, and Jun Rekimoto. 2014. Pixie Dust: Graphics Generated by Levitated and Animated Objects in Computational Acoustic-potential Field. *ACM Trans. Graph.* 33, 4, Article 85 (jul 2014), 13 pages. DOI:<http://dx.doi.org/10.1145/2601097.2601118>
  7. Romain Prévost, Moritz Bächer, Wojciech Jarosz, and Olga Sorkine-Hornung. 2016. Balancing 3D Models with Movable Masses. In *Proceedings of the Conference on Vision, Modeling and Visualization (VMV '16)*. Eurographics Association, Goslar Germany, Germany, 9–16. DOI:<http://dx.doi.org/10.2312/vmv.20161337>
  8. Romain Prévost, Emily Whiting, Sylvain Lefebvre, and Olga Sorkine-Hornung. 2013. Make It Stand: Balancing Shapes for 3D Fabrication. *ACM Trans. Graph.* 32, 4, Article 81 (jul 2013), 10 pages. DOI:<http://dx.doi.org/10.1145/2461912.2461957>
  9. Timothy Sun and Changxi Zheng. 2015. Computational Design of Twisty Joints and Puzzles. *ACM Trans. Graph.* 34, 4, Article 101 (July 2015), 11 pages. DOI:<http://dx.doi.org/10.1145/2766961>
  10. Nobuyuki Umetani, Yuki Koyama, Ryan Schmidt, and Takeo Igarashi. 2014. Pteromys: Interactive Design and Optimization of Free-formed Free-flight Model Airplanes. *ACM Trans. Graph.* 33, 4, Article 65 (July 2014), 10 pages. DOI:<http://dx.doi.org/10.1145/2601097.2601129>
  11. Nobuyuki Umetani, Jun Mitani, and Takeo Igarashi. 2010. Designing Custom-made Metallophone with Concurrent Eigenanalysis. In *NIME*.
  12. Nobuyuki Umetani, Athina Panotopoulou, Ryan Schmidt, and Emily Whiting. 2016. Print-one: Interactive Resonance Simulation for Free-form Print-wind Instrument Design. *ACM Trans. Graph.* 35, 6, Article 184 (Nov. 2016), 14 pages. DOI:<http://dx.doi.org/10.1145/2980179.2980250>
  13. L. Wang and E. Whiting. 2016. Buoyancy Optimization for Computational Fabrication. *Comput. Graph. Forum* 35, 2 (may 2016), 49–58. DOI:<http://dx.doi.org/10.1111/cgf.12810>
  14. Ran Zhang, Thomas Auzinger, Duygu Ceylan, Wilmot Li, and Bernd Bickel. 2017. Functionality-aware Retargeting of Mechanisms to 3D Shapes. *ACM Trans. Graph.* 36, 4, Article 81 (July 2017), 13 pages. DOI:<http://dx.doi.org/10.1145/3072959.3073710>
  15. Lifeng Zhu, Weiwei Xu, John Snyder, Yang Liu, Guoping Wang, and Baining Guo. 2012. Motion-guided Mechanical Toy Modeling. *ACM Trans. Graph.* 31, 6, Article 127 (Nov. 2012), 10 pages. DOI:<http://dx.doi.org/10.1145/2366145.2366146>